

# Introduction to Particle Accelerator Physics

## Tutorial 3 - Solutions

### 1. Dispersion Function

From the lecture recall the general solution of the dispersion function

$$D(s) = D_0 \cos \frac{s}{\rho} + D'_0 \rho \sin \frac{s}{\rho} + \rho \left( 1 - \cos \frac{s}{\rho} \right)$$

We can rewrite this and do a Taylor expansion of the sine and cosine functions keeping our limit  $\rho \rightarrow \infty$  in mind

$$\begin{aligned} D(s) &= D_0 \cos \frac{s}{\rho} + \rho - \rho \cos \frac{s}{\rho} + D'_0 \rho \sin \frac{s}{\rho} \\ &= D_0 \left( 1 - \frac{s^2}{2\rho^2} + - \dots \right) + \rho \left( 1 - 1 + \frac{s^2}{2\rho^2} - + \dots \right) + D'_0 \rho \left( \frac{s}{\rho} - \frac{s^3}{3! \cdot \rho^3} + - \dots \right) \\ &= D_0 (1 - \mathcal{O}(\rho^{-2})) + \mathcal{O}(\rho^{-1}) + D'_0 s + D'_0 \mathcal{O}(\rho^{-2}) \end{aligned}$$

And finally for a straight section we apply the limit  $\rho \rightarrow \infty$

$$\lim_{\rho \rightarrow \infty} D(s) = D_0 + D'_0 s$$

So if we enter a straight section with no dispersion at all ( $D_0 = D'_0 = 0$ ),  $D(s)$  will remain zero. In order to generate dispersion, we have to include a bend in our accelerator optics where  $\rho \neq 0$ .

### 2. Momentum Compaction Factor

From the lecture recall the definition of the momentum compaction factor

$$\frac{\Delta L}{L} = \alpha_c \cdot \frac{\Delta p}{p}$$

From this we can derive the maximum absolute change in path length

$$\Delta L = \alpha_c \cdot \frac{\Delta p}{p} \cdot L = \alpha_c \cdot \frac{\Delta p}{p} \cdot \frac{c}{f} = 6.3 \cdot 10^{-4} \cdot 9 \cdot 10^{-4} \cdot \frac{3 \cdot 10^8 \text{ m/s}}{1.04167 \cdot 10^6 \text{ Hz}} = 163 \text{ } \mu\text{m}$$

Compared to the circumference of 288m this is a very small path length variation.

### 3. Stability Criterion for a Circular Accelerator

a)

$$M_{Rev} = \begin{pmatrix} \cos \mu + \alpha_0 \sin \mu & \beta_0 \sin \mu \\ -\gamma_0 \sin \mu & \cos \mu - \alpha_0 \sin \mu \end{pmatrix}$$

Here we assume  $\alpha_0 = -\frac{\beta'_0}{2} = 0$  which gives  $\gamma_0 = -1/\beta_0$  and thus

$$M_{Rev} = \begin{pmatrix} \cos \mu & \beta_0 \sin \mu \\ -\frac{1}{\beta_0} \sin \mu & \cos \mu \end{pmatrix}$$

b) The betatron tune is defined as follows

$$Q = \frac{\mu}{2\pi} = \frac{\phi_{Rev}}{2\pi}$$

where the total phase advance in one revolution (accelerator circumference  $C$ ) is given by

$$\phi_{Rev} = \oint \frac{1}{\beta(s)} ds = \int_{s_0}^{s_0+C} \frac{1}{\beta(s)} ds$$

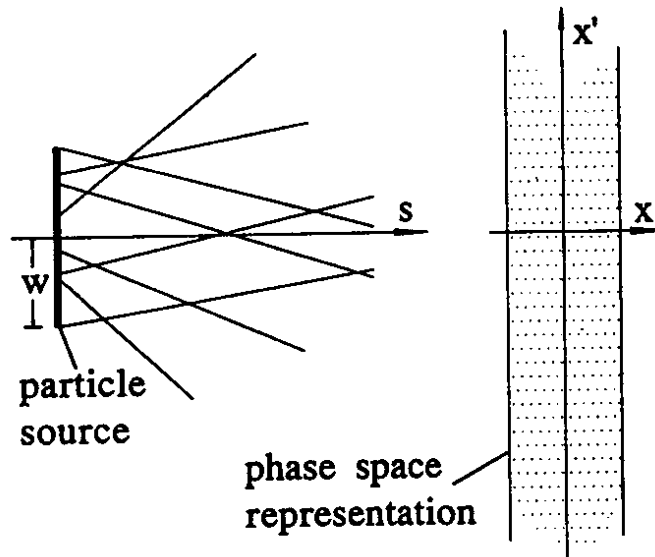
$M_{Rev}$  looks like a rotation matrix for the rotation angle  $\mu$ . The slight difference is the factor  $\beta_0$  respectively  $1/\beta_0$ . This leads to an ellipse in phase space. A point on this ellipse advances by the angle  $\mu$  for one revolution in the accelerator. The tune  $Q$  is the total betatron phase advance  $\mu$  divided by  $2\pi$ . Therefore  $Q$  is the number of betatron oscillations per revolution.

c) We can easily calculate the trace  $Tr(M_{Rev}) = 2 \cos \mu$  and since we know that the cos function has the co-domain  $[-1, +1]$  in  $\mathbb{R}$  we can derive a simple stability criterion

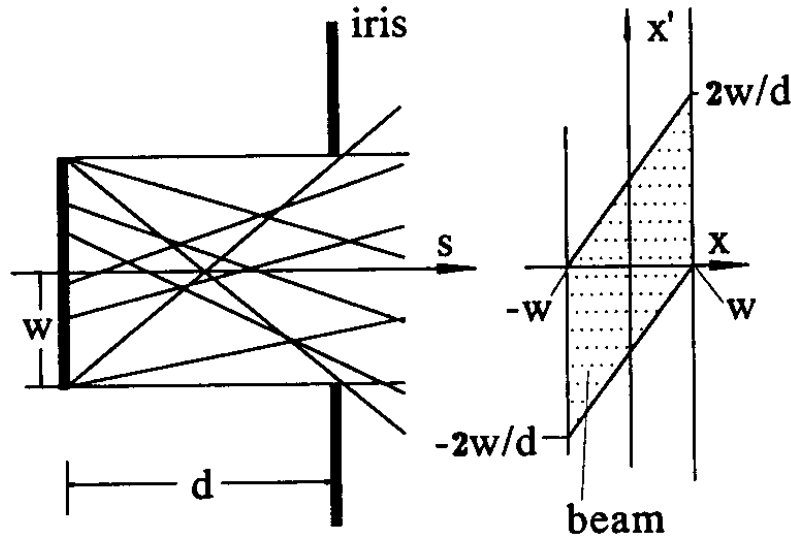
$$-1 \leq \frac{Tr(M_{Rev})}{2} \leq +1$$

#### 4. Phase Space Representations of Particle Sources

a) Particles are emitted from the entire source surface  $x \in [-w, +w]$  with a trajectory slope  $\phi \in [-\pi/2, +\pi/2]$ , i.e. the particles can have any  $x' \in \mathbb{R}$ . The occupied phase space area is infinite.



b) Particles with angle  $x' = 0$  are emitted from the entire source surface  $x \in [-w, +w]$  and arrive behind the iris opening. For  $x = \pm w$  there is a maximum angle  $x' = \pm 2w/d$  that will still be accepted by the iris. This leads to a parallelogram in phase space. Such a beam has a specific emittance given by the occupied phase space area.



## 5. Decapolar Magnetic Field

We chose the ansatz presented in the lecture

$$G_y(x) = \hat{g}x^4$$

where we have used a generic term proportional to the gradient

$$\hat{g} \propto \frac{d^4 G_y(x)}{dx^4}$$

Since we know

$$\nabla^2 \phi = \frac{\partial^2 \phi}{\partial x^2} + \frac{\partial^2 \phi}{\partial y^2} = \frac{d^2 G_y(x)}{dx^2} y + \frac{df(y)}{dy} = 0$$

we can derive  $f(y)$

$$\begin{aligned} \nabla^2 \phi &= \frac{d^2 G_y(x)}{dx^2} y + \frac{df(y)}{dy} = 0 \\ 12\hat{g}x^2 y + \frac{df(y)}{dy} &= 0 \\ \frac{df(y)}{dy} &= -12\hat{g}x^2 y \\ \implies f(y) &= -6\hat{g}x^2 y^2 \end{aligned}$$

The potential is then

$$\begin{aligned} \phi(x, y) &= G_y(x) y + \int f(y) dy \\ &= \hat{g}x^4 y - 2\hat{g}x^2 y^3 \end{aligned}$$

The equipotential lines are given by

$$x^4y - 2x^2y^3 = \text{const}$$

The magnetic induction is given by

$$\vec{B}(x, y) = \begin{pmatrix} \frac{\partial \phi}{\partial x} \\ \frac{\partial \phi}{\partial y} \end{pmatrix} = \begin{pmatrix} 4\hat{g}x^3y - 4\hat{g}xy^3 \\ \hat{g}x^4 - 6\hat{g}x^2y^2 \end{pmatrix}$$